



## Plate Load Test Results

Company Name  
Location  
Test Date  
Layer level

AL ANOD  
525+920  
20-07-2023  
P.S.G +0.50

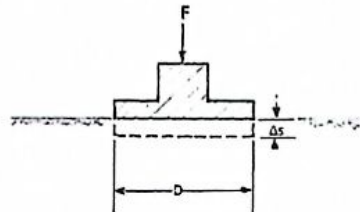
To 526+000

Station 525+950

### EQUIPMENT AND TEST PROCEDURE :-

The basis of the given equation is Boussinesq's theory of the relationship between the modulus of elasticity and the settlement of a circular rigid plate with the diameter  $D$ .

The load is applied to a circular rigid steel bearing plate by a hydraulic jack in several steps. The settlement under each load step is recorded. The following sketch shows the principle of the test.



$F$  = load

$\Delta s$  = settlement

$D$  = diameter of the plate

The diameter  $D$  of the plate is generally 0.30 m. For very coarse grained material also plates with diameter  $D = 0.60$  m and  $D = 0.762$  m are used

The load is applied in 6 load increments of equal size. Under each load step the settlement must come to a noticeable end ( $< 0.02$  mm/minute). After the maximum load is reached the unloading procedure can begin. After that, the plate is reloaded in 5 steps. A loaded truck, an excavator or a roller usually serve as counterweight for the hydraulic jack

Diameter = 300mm

| Loading   | Load  | Load   | Stress | Dial 1 | Dial 2 | Dial 3 | Sett. 1 | Sett. 2 | Sett. 3 | Avg. Sett. |
|-----------|-------|--------|--------|--------|--------|--------|---------|---------|---------|------------|
| Stage No. | Bar   | KN     | MN/M2  | mm     | mm     | mm     | mm      | mm      | mm      | mm         |
| 0.000     | 0.0   | 0.000  | 0.00   | 20.00  | 20.00  |        | 0.000   | 0.000   |         | 0.000      |
| 1.000     | 2.1   | 0.707  | 0.01   | 19.95  | 19.96  |        | 0.050   | 0.040   |         | 0.045      |
| 2.000     | 17.1  | 5.652  | 0.08   | 19.85  | 19.84  |        | 0.150   | 0.160   |         | 0.155      |
| 0.080     | 34.2  | 11.304 | 0.16   | 19.72  | 19.70  |        | 0.280   | 0.300   |         | 0.290      |
| 4.000     | 53.3  | 17.663 | 0.25   | 19.50  | 19.59  |        | 0.500   | 0.410   |         | 0.455      |
| 5.000     | 70.5  | 23.315 | 0.33   | 19.25  | 19.48  |        | 0.750   | 0.520   |         | 0.635      |
| 6.000     | 89.8  | 29.673 | 0.42   | 19.02  | 19.36  |        | 0.980   | 0.640   |         | 0.810      |
| 7.000     | 106.8 | 35.325 | 0.50   | 18.84  | 19.29  |        | 1.160   | 0.710   |         | 0.935      |
| 8.000     | 53.4  | 17.663 | 0.25   | 18.89  | 19.31  |        | 1.110   | 0.690   |         | 0.900      |
| 9.000     | 26.7  | 8.831  | 0.12   | 19.01  | 19.40  |        | 0.990   | 0.600   |         | 0.795      |
| 9.000     | 2.1   | 0.707  | 0.01   | 19.31  | 19.60  |        | 0.690   | 0.400   |         | 0.545      |
| 10.000    | 2.1   | 0.707  | 0.01   | 19.31  | 19.60  |        | 0.690   | 0.400   |         | 0.545      |
| 11.000    | 17.1  | 5.652  | 0.08   | 19.28  | 19.55  |        | 0.720   | 0.450   |         | 0.585      |
| 12.000    | 34.2  | 11.304 | 0.16   | 19.12  | 19.46  |        | 0.880   | 0.540   |         | 0.710      |
| 13.000    | 53.3  | 17.663 | 0.25   | 19.00  | 19.40  |        | 1.000   | 0.600   |         | 0.800      |
| 14.000    | 70.5  | 23.315 | 0.33   | 18.94  | 19.35  |        | 1.060   | 0.650   |         | 0.855      |
| 15.000    | 89.8  | 29.673 | 0.42   | 18.85  | 19.30  |        | 1.150   | 0.700   |         | 0.925      |

|                    |         | s       | ΔS      | Δσ  |
|--------------------|---------|---------|---------|-----|
| 0.7 σ <sub>1</sub> | 0.35    | 0.70063 | 0.4275  | 0.2 |
| 0.3 σ <sub>1</sub> | 0.15    | 0.27313 |         |     |
| 0.7 σ <sub>2</sub> | 0.35    | 0.87056 | 0.24555 | 0.2 |
| 0.3 σ <sub>2</sub> | 0.15    | 0.625   |         |     |
| D (mm)             | 300     |         |         |     |
| Ev <sub>1</sub>    | 105.26  |         |         |     |
| Ev <sub>2</sub>    | 183.26  |         |         |     |
| Area ( Sq.m)       | 0.07065 |         |         |     |

|                                  |      |  |  |
|----------------------------------|------|--|--|
| Ev <sub>2</sub> /Ev <sub>1</sub> | 1.74 |  |  |
|----------------------------------|------|--|--|

$$E_s = 0.75 \cdot D \cdot \Delta \sigma / \Delta s$$

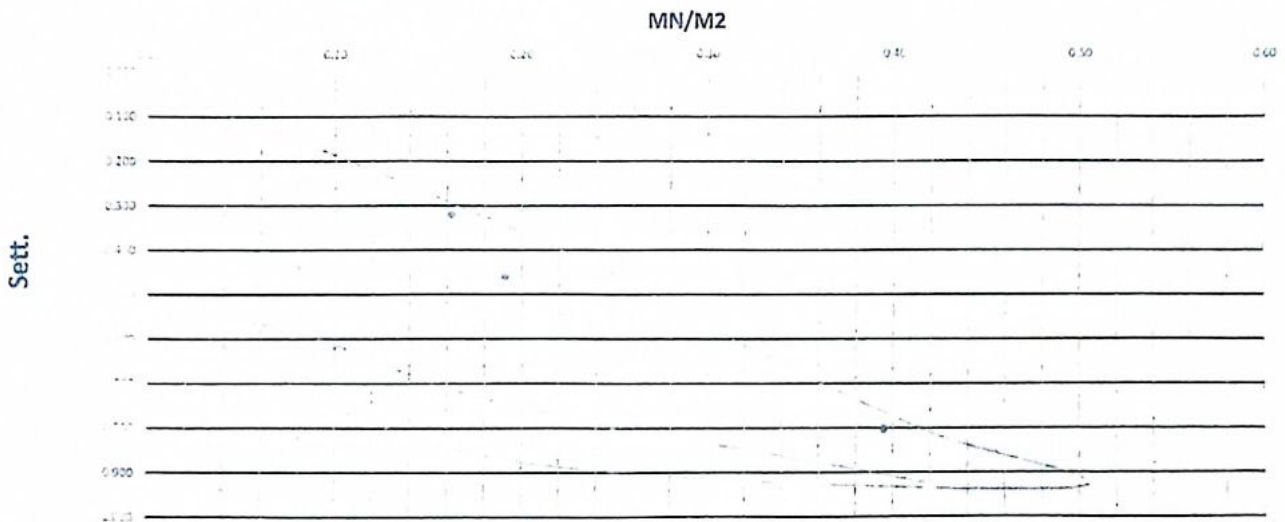
$E_s$  = deformation modulus

$\Delta s$  = load increment

$\Delta \sigma$  = settlement increment

$D$  = diameter of the plate, generally 0.30 m

For this calculation  $\Delta\sigma$  and  $\Delta\epsilon$  are usually taken from the load span between  $0.3 \sigma_{max}$  and  $0.7 \sigma_{max}$ .



Lab. Specialist

Name : *Hassan*

Sign : *[Signature]*

Lab. Engineer

Name : *[Signature]*

Sign : *[Signature]*

Consultant Engineer

Name : Hassan

Sign : *[Signature]* 25/7/2023

## Plate Load Test Results

Company Name

AL ANOD

Location

525+920

To

526+000

Station

525+975

Test Date

20-07-2023

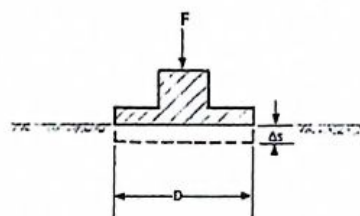
Layer level

P.S.G +0.50

### EQUIPMENT AND TEST PROCEDURE :-

The basis of the given equation is Boussinesq's theory of the relationship between the modulus of elasticity and the settlement of a circular rigid plate with the diameter  $D$ .

The load is applied to a circular rigid steel bearing plate by a hydraulic jack in several steps. The settlement under each load step is recorded. The following sketch shows the principle of the test.



$F$  = load

$\Delta s$  = settlement

$D$  = diameter of the plate

The diameter  $D$  of the plate is generally 0.30 m. For very coarse grained material also plates with diameter  $D = 0.60$  m and  $D = 0.762$  m are used

The load is applied in 6 load increments of equal size. Under each load step the settlement must come to a noticeable end ( $< 0.02$  mm/minute). After the maximum load is reached the unloading procedure can begin. After that, the plate is reloaded in 5 steps. A loaded truck, an excavator or a roller usually serve as counterweight for the hydraulic jack

Diameter = 300mm

| Loading   | Load  | Load   | Stress | Dial 1 | Dial 2 | Dial 3 | Sett. 1 | Sett. 2 | Sett. 3 | Avg. Sett. |
|-----------|-------|--------|--------|--------|--------|--------|---------|---------|---------|------------|
| Stage No. | Bar   | KN     | MM/M2  | mm     | mm     | mm     | mm      | mm      | mm      | mm         |
| 0.000     | 0.0   | 0.000  | 0.00   | 20.00  | 20.00  |        | 0.000   | 0.000   |         | 0.000      |
| 1.000     | 2.1   | 0.707  | 0.01   | 19.90  | 19.85  |        | 0.100   | 0.150   |         | 0.125      |
| 2.000     | 17.1  | 5.652  | 0.08   | 19.62  | 19.56  |        | 0.380   | 0.440   |         | 0.410      |
| 3.000     | 34.2  | 11.304 | 0.16   | 19.55  | 19.20  |        | 0.450   | 0.800   |         | 0.625      |
| 4.000     | 53.3  | 17.663 | 0.25   | 19.44  | 18.95  |        | 0.560   | 1.050   |         | 0.805      |
| 5.000     | 70.5  | 23.315 | 0.33   | 19.34  | 18.75  |        | 0.660   | 1.250   |         | 0.955      |
| 6.000     | 89.8  | 29.673 | 0.42   | 19.29  | 18.52  |        | 0.710   | 1.480   |         | 1.095      |
| 7.000     | 106.8 | 35.325 | 0.50   | 19.20  | 18.35  |        | 0.800   | 1.650   |         | 1.225      |
| 8.000     | 53.4  | 17.663 | 0.25   | 19.25  | 18.40  |        | 0.750   | 1.600   |         | 1.175      |
| 9.000     | 26.7  | 8.831  | 0.12   | 19.30  | 18.48  |        | 0.700   | 1.520   |         | 1.110      |
| 9.000     | 2.1   | 0.707  | 0.01   | 19.35  | 18.64  |        | 0.650   | 1.360   |         | 1.005      |
| 10.000    | 2.1   | 0.707  | 0.01   | 19.35  | 18.64  |        | 0.650   | 1.360   |         | 1.005      |
| 11.000    | 17.1  | 5.652  | 0.08   | 19.32  | 18.62  |        | 0.680   | 1.380   |         | 1.030      |
| 12.000    | 34.2  | 11.304 | 0.16   | 19.28  | 18.52  |        | 0.720   | 1.480   |         | 1.100      |
| 13.000    | 53.3  | 17.663 | 0.25   | 19.24  | 18.45  |        | 0.760   | 1.550   |         | 1.155      |
| 14.000    | 70.5  | 23.315 | 0.33   | 19.22  | 18.41  |        | 0.780   | 1.590   |         | 1.185      |
| 15.000    | 89.8  | 29.673 | 0.42   | 19.19  | 18.38  |        | 0.810   | 1.620   |         | 1.215      |

|                |         | $\epsilon$ | $\Delta S$ | $\Delta \sigma$ |
|----------------|---------|------------|------------|-----------------|
| 0.7 $\sigma_1$ | 0.35    | 0.98125    | 0.38313    | 0.2             |
| 0.3 $\sigma_1$ | 0.15    | 0.59813    |            |                 |
| 0.7 $\sigma_2$ | 0.35    | 1.19167    | 0.13666    | 0.2             |
| 0.3 $\sigma_2$ | 0.15    | 1.055      |            |                 |
| D (mm)         | 300     |            |            |                 |
| $E_{v1}$       | 117.46  |            |            |                 |
| $E_{v2}$       | 329.27  |            |            |                 |
| Area (Sq.m)    | 0.07065 |            |            |                 |

|                 |      |  |  |
|-----------------|------|--|--|
| $E_{v2}/E_{v1}$ | 2.80 |  |  |
|-----------------|------|--|--|

$$E_v = 0.75 \cdot D \cdot \Delta \sigma / \Delta s$$

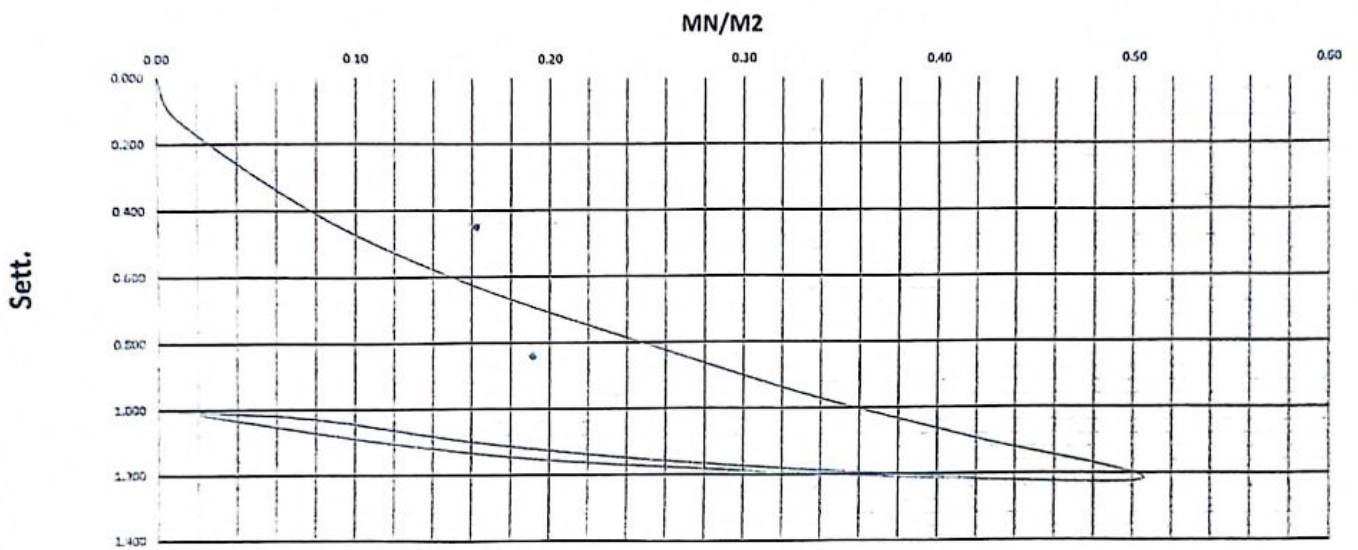
$E_v$  = deformation modulus

$D$  = load increment

$\Delta s$  = settlement increment

$D$  = diameter of the plate, generally 0.30 m

For this calculation  $\Delta\sigma$  and  $\Delta\varepsilon$  are usually taken from the load span between  $0.3 \sigma_{max}$  and  $0.7 \sigma_{max}$ .



Lab. Specialist

Name : *M. H. S. S.*

Sign : *M. H. S. S.*

Lab. Engineer

Name : *Eng. H. S. S.*

Sign : *Eng. H. S. S.*

Consultant Engineer

Name : *Hassan*

Sign : *25/7/2023*



Owner Consultant



Contractor Consultant



Contractor



Owner



## Plate Load Test Results

Company Name

AL ANOD

Location

525+920

To

526+000

Station

525+925

Test Date

20-07-2023

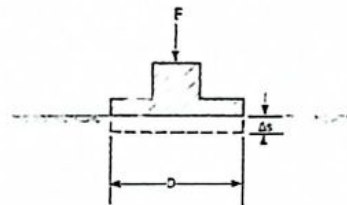
Layer level

P.S.G +0.50

### EQUIPMENT AND TEST PROCEDURE :-

The basis of the given equation is Boussinesq's theory of the relationship between the modulus of elasticity and the settlement of a circular rigid plate with the diameter  $D$ .

The load is applied to a circular rigid steel bearing plate by a hydraulic jack in several steps. The settlement under each load step is recorded. The following sketch shows the principle of the test.



$F$  = load

$\Delta s$  = settlement

$D$  = diameter of the plate

The diameter  $D$  of the plate is generally 0.30 m. For very coarse grained material also plates with diameter  $D = 0.60$  m and  $D = 0.762$  m are used.

The load is applied in 6 load increments of equal size. Under each load step the settlement must come to a noticeable end ( $< 0.02$  mm/minute). After the maximum load is reached the unloading procedure can begin. After that, the plate is reloaded in 5 steps. A loaded truck, an excavator or a roller usually serve as counterweight for the hydraulic jack.

Diameter = 300mm

| Loading   | Load  | Load   | Stress | Dial 1 | Dial 2 | Dial 3 | Sett. 1 | Sett. 2 | Sett. 3 | Ave. Sett. |
|-----------|-------|--------|--------|--------|--------|--------|---------|---------|---------|------------|
| Stage No. | Bar   | KN     | MIN/M2 | mm     | mm     | mm     | mm      | mm      | mm      | mm         |
| 0.000     | 0.0   | 0.000  | 0.00   | 20.00  | 20.00  |        | 0.000   | 0.000   |         | 0.000      |
| 1.000     | 2.1   | 0.707  | 0.01   | 19.94  | 19.94  |        | 0.060   | 0.060   |         | 0.060      |
| 2.000     | 17.1  | 5.652  | 0.08   | 19.84  | 19.83  |        | 0.160   | 0.170   |         | 0.165      |
| 3.000     | 34.2  | 11.304 | 0.16   | 19.70  | 19.67  |        | 0.300   | 0.330   |         | 0.315      |
| 4.000     | 53.3  | 17.663 | 0.25   | 19.48  | 19.58  |        | 0.520   | 0.420   |         | 0.470      |
| 5.000     | 70.5  | 23.315 | 0.33   | 19.23  | 19.47  |        | 0.770   | 0.530   |         | 0.650      |
| 6.000     | 89.8  | 29.673 | 0.42   | 19.00  | 19.35  |        | 1.000   | 0.650   |         | 0.825      |
| 7.000     | 106.8 | 35.325 | 0.50   | 18.83  | 19.27  |        | 1.170   | 0.730   |         | 0.950      |
| 8.000     | 53.4  | 17.663 | 0.25   | 18.90  | 19.32  |        | 1.100   | 0.680   |         | 0.890      |
| 9.000     | 26.7  | 8.831  | 0.12   | 19.01  | 19.41  |        | 0.990   | 0.590   |         | 0.790      |
| 9.000     | 2.1   | 0.707  | 0.01   | 19.32  | 19.62  |        | 0.680   | 0.380   |         | 0.530      |
| 10.000    | 2.1   | 0.707  | 0.01   | 19.32  | 19.62  |        | 0.680   | 0.380   |         | 0.530      |
| 11.000    | 17.1  | 5.652  | 0.08   | 19.27  | 19.54  |        | 0.730   | 0.460   |         | 0.595      |
| 12.000    | 34.2  | 11.304 | 0.16   | 19.13  | 19.47  |        | 0.870   | 0.530   |         | 0.700      |
| 13.000    | 53.3  | 17.663 | 0.25   | 19.02  | 19.40  |        | 0.980   | 0.600   |         | 0.790      |
| 14.000    | 70.5  | 23.315 | 0.33   | 18.94  | 19.36  |        | 1.060   | 0.640   |         | 0.850      |
| 15.000    | 89.8  | 29.673 | 0.42   | 18.85  | 19.32  |        | 1.150   | 0.680   |         | 0.915      |

|                |         | $\sigma$ | $\Delta s$ | $\Delta \sigma$ |
|----------------|---------|----------|------------|-----------------|
| 0.7 $\sigma_1$ | 0.35    | 0.71562  | 0.41937    | 0.2             |
| 0.3 $\sigma_1$ | 0.15    | 0.29625  |            |                 |
| 0.7 $\sigma_2$ | 0.35    | 0.86444  | 0.20444    | 0.2             |
| 0.3 $\sigma_2$ | 0.15    | 0.66001  |            |                 |
| D (mm)         | 300     |          |            |                 |
| $E_{v1}$       | 107.30  |          |            |                 |
| $E_{v2}$       | 220.12  |          |            |                 |
| Area (Sq.m)    | 0.07065 |          |            |                 |

|                 |      |  |  |
|-----------------|------|--|--|
| $E_{v2}/E_{v1}$ | 2.05 |  |  |
|-----------------|------|--|--|

$$E_v = 0.75 \cdot D \cdot \Delta \sigma / \Delta s$$

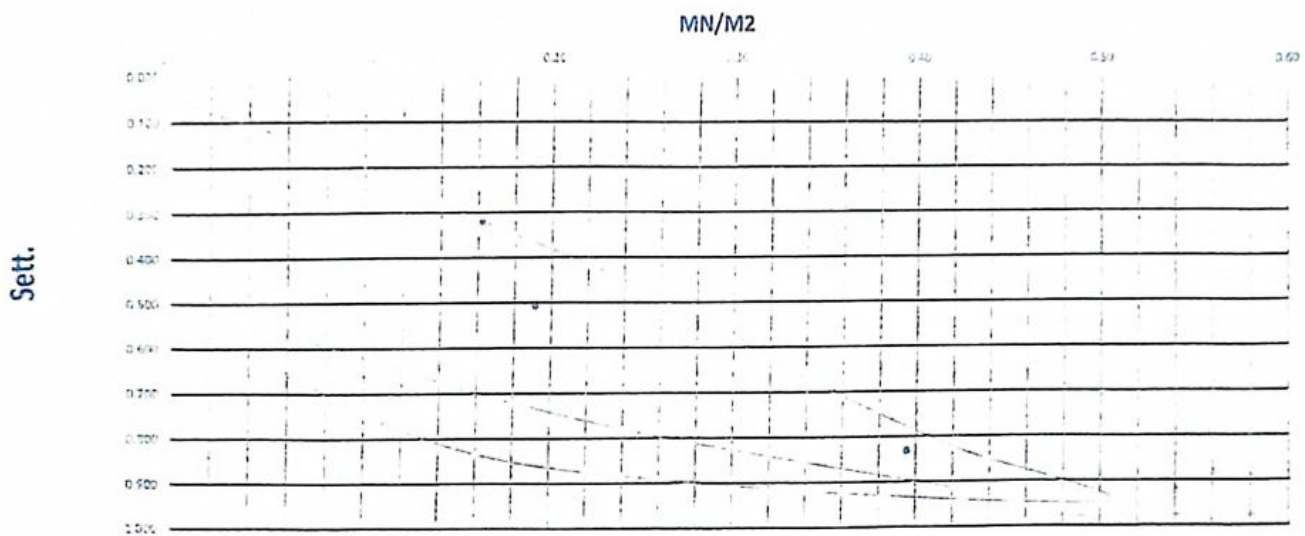
$E_v$  = deformation modulus

$\Delta \sigma$  = load increment

$\Delta s$  = settlement increment

$D$  = diameter of the plate, generally 0.30 m

For this calculation  $\Delta\sigma$  and  $\Delta\epsilon$  are usually taken from the load span between  $0.3 \sigma_{max}$  and  $0.7 \sigma_{max}$ .



Lab. Specialist  
Name : M. S. S. S.  
Sign : [Signature]

Lab. Engineer  
Name : [Signature]  
Sign : [Signature]

Consultant Engineer  
Name : Hassan  
Sign : [Signature]



## Plate Load Test Results

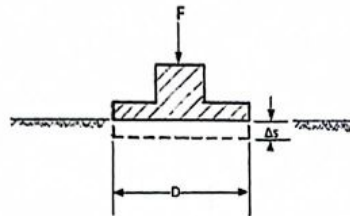
|              |                   |    |         |
|--------------|-------------------|----|---------|
| Company Name | AL ANOD           |    |         |
| Location     | 525+920           | To | 526+000 |
| Test Date    | 13-08-2023        |    |         |
| Layer level  | sub ballast +0.90 |    |         |

|         |         |
|---------|---------|
| Station | 525+935 |
|---------|---------|

### EQUIPMENT AND TEST PROCEDURE :-

The basis of the given equation is Boussinesq's theory of the relationship between the modulus of elasticity and the settlement of a circular rigid plate with the diameter  $D$ .

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Diameter = 300mm

| Loading   | Load  | Load   | Stress | Dial 1 | Dial 2 | Dial 3 | Sett. 1 | Sett. 2 | Sett. 3 | Avg. Sett. |
|-----------|-------|--------|--------|--------|--------|--------|---------|---------|---------|------------|
| Stage No. | Bar   | KN     | MN/M2  | mm     | mm     | mm     | mm      | mm      | mm      | mm         |
| 0.000     | 0.0   | 0.000  | 0.00   | 20.00  | 20.00  |        | 0.000   | 0.000   |         | 0.000      |
| 1.000     | 2.1   | 0.707  | 0.01   | 19.95  | 19.65  |        | 0.050   | 0.350   |         | 0.200      |
| 2.000     | 17.1  | 5.652  | 0.08   | 19.70  | 19.30  |        | 0.300   | 0.700   |         | 0.500      |
| 0.080     | 34.2  | 11.304 | 0.16   | 19.55  | 19.09  |        | 0.450   | 0.910   |         | 0.680      |
| 4.000     | 53.3  | 17.663 | 0.25   | 19.41  | 18.92  |        | 0.590   | 1.080   |         | 0.835      |
| 5.000     | 70.5  | 23.315 | 0.33   | 19.31  | 18.78  |        | 0.690   | 1.220   |         | 0.955      |
| 6.000     | 89.8  | 29.673 | 0.42   | 19.20  | 18.60  |        | 0.800   | 1.400   |         | 1.100      |
| 7.000     | 106.8 | 35.325 | 0.50   | 19.10  | 18.50  |        | 0.900   | 1.500   |         | 1.200      |
| 8.000     | 53.4  | 17.663 | 0.25   | 19.19  | 18.60  |        | 0.810   | 1.400   |         | 1.105      |
| 9.000     | 26.7  | 8.831  | 0.12   | 19.25  | 18.66  |        | 0.750   | 1.340   |         | 1.045      |
| 9.000     | 2.1   | 0.707  | 0.01   | 19.35  | 18.82  |        | 0.650   | 1.180   |         | 0.915      |
| 10.000    | 2.1   | 0.707  | 0.01   | 19.35  | 18.82  |        | 0.650   | 1.180   |         | 0.915      |
| 11.000    | 17.1  | 5.652  | 0.08   | 19.31  | 18.77  |        | 0.690   | 1.230   |         | 0.960      |
| 12.000    | 34.2  | 11.304 | 0.16   | 19.25  | 18.66  |        | 0.750   | 1.340   |         | 1.045      |
| 13.000    | 53.3  | 17.663 | 0.25   | 19.21  | 18.61  |        | 0.790   | 1.390   |         | 1.090      |
| 14.000    | 70.5  | 23.315 | 0.33   | 19.17  | 18.57  |        | 0.830   | 1.430   |         | 1.130      |
| 15.000    | 89.8  | 29.673 | 0.42   | 19.10  | 18.50  |        | 0.900   | 1.500   |         | 1.200      |

|                    |         | s       | Δs      | Δσ  |
|--------------------|---------|---------|---------|-----|
| 0.7 σ <sub>1</sub> | 0.35    | 1.0125  | 0.355   | 0.2 |
| 0.3 σ <sub>1</sub> | 0.15    | 0.6575  |         |     |
| 0.7 σ <sub>2</sub> | 0.35    | 1.14556 | 0.14055 | 0.2 |
| 0.3 σ <sub>2</sub> | 0.15    | 1.005   |         |     |
| D (mm)             | 300     |         |         |     |
| E <sub>v1</sub>    | 126.76  |         |         |     |
| E <sub>v2</sub>    | 320.17  |         |         |     |
| Area ( Sq.m)       | 0.07065 |         |         |     |

|                                  |      |  |  |
|----------------------------------|------|--|--|
| E <sub>v2</sub> /E <sub>v1</sub> | 2.53 |  |  |
|----------------------------------|------|--|--|

$$E_v = 4.75 \cdot D \cdot \Delta \sigma / \Delta s$$

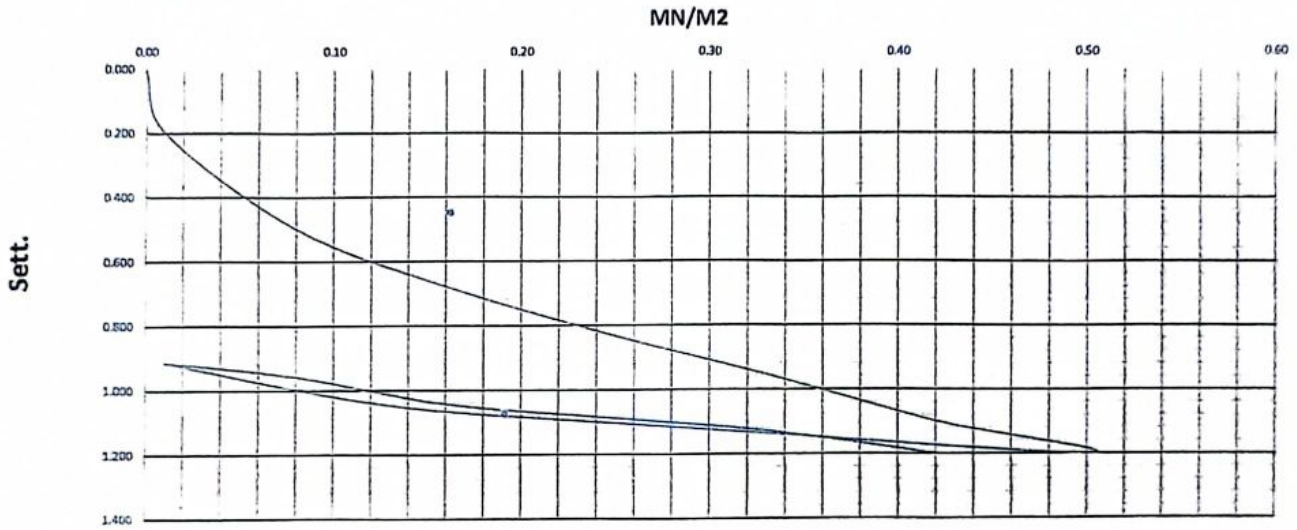
$E_v$  = deformation modulus

$\Delta \sigma$  = load increment

$\Delta s$  = settlement increment

$D$  = diameter of the plate, generally 0.30 m

For this calculation  $\Delta\sigma$  and  $\Delta s$  are usually taken from the load span between  $0.3 \sigma_{max}$  and  $0.7 \sigma_{max}$ .



Lab. Specialist

Name :

Sign :

Lab. Engineer

Name : Ahmed Hajeem

Sign :

Consultant Engineer

Name : Hassan

Sign :

16/8/2023

## Plate Load Test Results

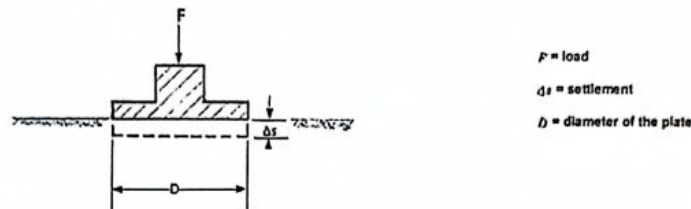
|              |                   |    |         |
|--------------|-------------------|----|---------|
| Company Name | AL ANOD           |    |         |
| Location     | 525+920           | To | 526+000 |
| Test Date    | 13-08-2023        |    |         |
| Layer level  | sub ballast +0.90 |    |         |

|         |         |
|---------|---------|
| Station | 525+955 |
|---------|---------|

### EQUIPMENT AND TEST PROCEDURE :-

The basis of the given equation is Boussinesq's theory of the relationship between the modulus of elasticity and the settlement of a circular rigid plate with the diameter  $D$ .

The load is applied to a circular rigid steel bearing plate by a hydraulic jack in several steps. The settlement under each load step is recorded. The following sketch shows the principle of the test.



The diameter  $D$  of the plate is generally 0.30 m. For very coarse grained material also plates with diameter  $D = 0.60$  m and  $D = 0.762$  m are used.

The load is applied in 6 load increments of equal size. Under each load step the settlement must come to a noticeable end ( $< 0.02$  mm/minute). After the maximum load is reached the unloading procedure can begin. After that, the plate is reloaded in 5 steps. A loaded truck, an excavator or a roller usually serve as counterweight for the hydraulic jack.

Diameter = 300mm

| Loading   | Load  | Load   | Stress | Dial 1 | Dial 2 | Dial 3 | Sett. 1 | Sett. 2 | Sett. 3 | Avg. Sett. |
|-----------|-------|--------|--------|--------|--------|--------|---------|---------|---------|------------|
| Stage No. | Bar   | KN     | MM/M2  | mm     | mm     | mm     | mm      | mm      | mm      | mm         |
| 0.000     | 0.0   | 0.000  | 0.00   | 20.00  | 20.00  |        | 0.000   | 0.000   |         | 0.000      |
| 1.000     | 2.1   | 0.707  | 0.01   | 19.99  | 19.96  |        | 0.010   | 0.040   |         | 0.025      |
| 2.000     | 17.1  | 5.652  | 0.08   | 19.84  | 19.82  |        | 0.160   | 0.180   |         | 0.170      |
| 0.080     | 34.2  | 11.304 | 0.16   | 19.80  | 19.65  |        | 0.200   | 0.350   |         | 0.275      |
| 4.000     | 53.3  | 17.663 | 0.25   | 19.76  | 19.44  |        | 0.240   | 0.560   |         | 0.400      |
| 5.000     | 70.5  | 23.315 | 0.33   | 19.66  | 19.20  |        | 0.340   | 0.800   |         | 0.570      |
| 6.000     | 89.8  | 29.673 | 0.42   | 19.60  | 19.02  |        | 0.400   | 0.980   |         | 0.690      |
| 7.000     | 106.8 | 35.325 | 0.50   | 19.55  | 18.80  |        | 0.450   | 1.200   |         | 0.825      |
| 8.000     | 53.4  | 17.663 | 0.25   | 19.60  | 18.93  |        | 0.400   | 1.070   |         | 0.735      |
| 9.000     | 26.7  | 8.831  | 0.12   | 19.80  | 19.05  |        | 0.200   | 0.950   |         | 0.575      |
| 9.000     | 2.1   | 0.707  | 0.01   | 19.89  | 19.33  |        | 0.110   | 0.670   |         | 0.390      |
| 10.000    | 2.1   | 0.707  | 0.01   | 19.89  | 19.33  |        | 0.110   | 0.670   |         | 0.390      |
| 11.000    | 17.1  | 5.652  | 0.08   | 19.86  | 19.23  |        | 0.140   | 0.770   |         | 0.455      |
| 12.000    | 34.2  | 11.304 | 0.16   | 19.80  | 19.12  |        | 0.200   | 0.880   |         | 0.540      |
| 13.000    | 53.3  | 17.663 | 0.25   | 19.76  | 19.01  |        | 0.240   | 0.990   |         | 0.615      |
| 14.000    | 70.5  | 23.315 | 0.33   | 19.71  | 18.95  |        | 0.290   | 1.050   |         | 0.670      |
| 15.000    | 89.8  | 29.673 | 0.42   | 19.60  | 18.90  |        | 0.400   | 1.100   |         | 0.750      |

|                |         | s       | Δs      | Δσ  |
|----------------|---------|---------|---------|-----|
| 0.7 $\sigma_1$ | 0.35    | 0.57188 | 0.31    | 0.2 |
| 0.3 $\sigma_1$ | 0.15    | 0.26188 |         |     |
| 0.7 $\sigma_2$ | 0.35    | 0.68778 | 0.16777 | 0.2 |
| 0.3 $\sigma_2$ | 0.15    | 0.52001 |         |     |
| D (mm)         | 300     |         |         |     |
| $E_{v1}$       | 145.16  |         |         |     |
| $E_{v2}$       | 268.22  |         |         |     |
| Area (Sq.m)    | 0.07065 |         |         |     |

|                 |      |
|-----------------|------|
| $E_{v2}/E_{v1}$ | 1.85 |
|-----------------|------|

$$E_v = 0.75 \cdot D \cdot \Delta\sigma / \Delta s$$

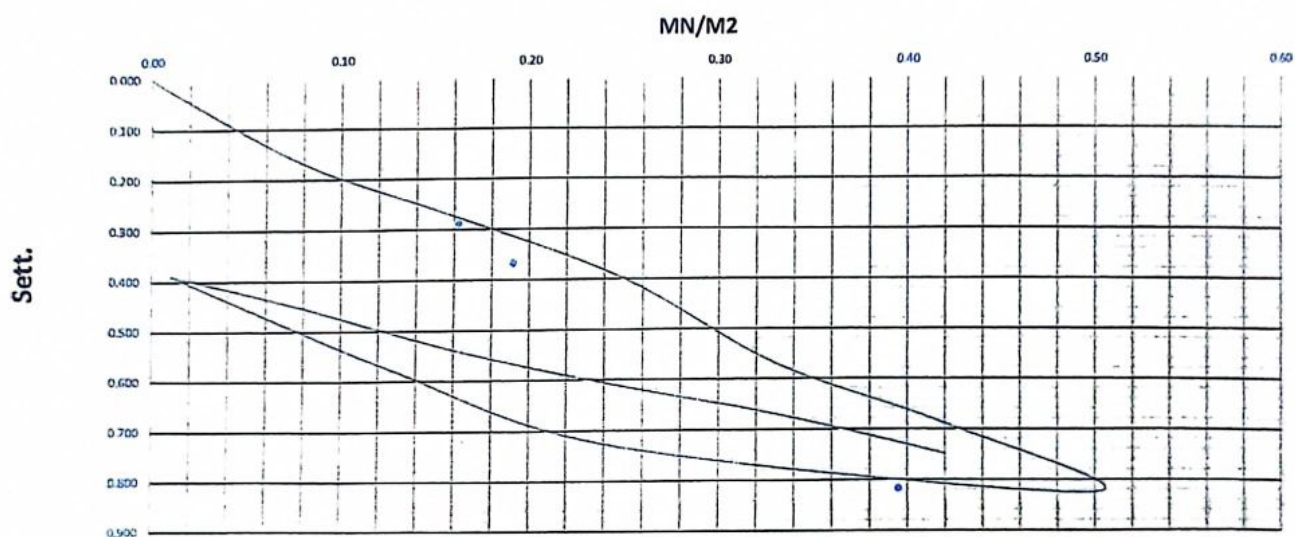
$E_v$  = deformation modulus

$\Delta\sigma$  = load increment

$\Delta s$  = settlement increment

$D$  = diameter of the plate, generally 0.30 m

For this calculation  $\Delta\sigma$  and  $\Delta s$  are usually taken from the load span between  $0.3 \sigma_{max}$  and  $0.7 \sigma_{max}$ .



Lab. Specialist

Name :

Sign :

Lab. Engineer

Name : Ahmed Hajeem

Sign :

*[Handwritten signature of Ahmed Hajeem]*

Consultant Engineer

Name : Hassan

Sign :

*[Handwritten signature of Hassan]*  
16/8/2023

## Plate Load Test Results

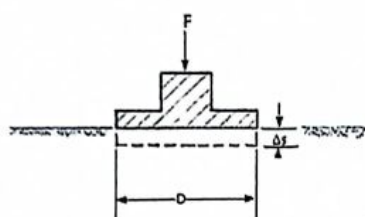
|              |                   |    |         |
|--------------|-------------------|----|---------|
| Company Name | AL ANOD           |    |         |
| Location     | 525+920           | To | 526+000 |
| Test Date    | 13-08-2023        |    |         |
| Layer level  | sub ballast +0.90 |    |         |

|         |         |
|---------|---------|
| Station | 525+970 |
|---------|---------|

### EQUIPMENT AND TEST PROCEDURE :-

The basis of the given equation is Boussinesq's theory of the relationship between the modulus of elasticity and the settlement of a circular rigid plate with the diameter  $D$ .

The load is applied to a circular rigid steel bearing plate by a hydraulic jack in several steps. The settlement under each load step is recorded. The following sketch shows the principle of the test.



$F$  = load  
 $ds$  = settlement  
 $D$  = diameter of the plate

The diameter  $D$  of the plate is generally 0.30 m. For very coarse grained material also plates with diameter  $D = 0.60$  m and  $D = 0.762$  m are used.

The load is applied in 6 load increments of equal size. Under each load step the settlement must come to a noticeable end ( $< 0.02$  mm/minute). After the maximum load is reached the unloading procedure can begin. After that, the plate is reloaded in 5 steps. A loaded truck, an excavator or a roller usually serve as counterweight for the hydraulic jack.

Diameter = 300mm

| Loading   | Load  | Load   | Stress | Dial 1 | Dial 2 | Dial 3 | Sett. 1 | Sett. 2 | Sett. 3 | Avg. Sett. |
|-----------|-------|--------|--------|--------|--------|--------|---------|---------|---------|------------|
| Stage No. | Bar   | KN     | MIN/M2 | mm     | mm     | mm     | mm      | mm      | mm      | mm         |
| 0.000     | 0.0   | 0.000  | 0.00   | 20.00  | 20.00  |        | 0.000   | 0.000   |         | 0.000      |
| 1.000     | 2.1   | 0.707  | 0.01   | 19.84  | 19.90  |        | 0.160   | 0.100   |         | 0.130      |
| 2.000     | 17.1  | 5.652  | 0.08   | 19.50  | 19.79  |        | 0.500   | 0.210   |         | 0.355      |
| 3.000     | 34.2  | 11.304 | 0.16   | 19.20  | 19.59  |        | 0.800   | 0.410   |         | 0.605      |
| 4.000     | 53.3  | 17.663 | 0.25   | 19.07  | 19.41  |        | 0.930   | 0.590   |         | 0.760      |
| 5.000     | 70.5  | 23.315 | 0.33   | 18.85  | 19.24  |        | 1.150   | 0.760   |         | 0.955      |
| 6.000     | 89.8  | 29.673 | 0.42   | 18.68  | 19.18  |        | 1.320   | 0.820   |         | 1.070      |
| 7.000     | 106.8 | 35.325 | 0.50   | 18.55  | 19.00  |        | 1.450   | 1.000   |         | 1.225      |
| 8.000     | 53.4  | 17.663 | 0.25   | 18.60  | 19.03  |        | 1.400   | 0.970   |         | 1.185      |
| 9.000     | 26.7  | 8.831  | 0.12   | 18.70  | 19.08  |        | 1.300   | 0.920   |         | 1.110      |
| 10.000    | 2.1   | 0.707  | 0.01   | 18.85  | 19.14  |        | 1.150   | 0.860   |         | 1.005      |
| 11.000    | 2.1   | 0.707  | 0.01   | 18.85  | 19.14  |        | 1.150   | 0.860   |         | 1.005      |
| 12.000    | 17.1  | 5.652  | 0.08   | 18.83  | 19.13  |        | 1.170   | 0.870   |         | 1.020      |
| 13.000    | 34.2  | 11.304 | 0.16   | 18.78  | 19.09  |        | 1.220   | 0.910   |         | 1.065      |
| 14.000    | 53.3  | 17.663 | 0.25   | 18.70  | 19.07  |        | 1.300   | 0.930   |         | 1.115      |
| 15.000    | 70.5  | 23.315 | 0.33   | 18.64  | 19.05  |        | 1.360   | 0.950   |         | 1.155      |
| 16.000    | 89.8  | 29.673 | 0.42   | 18.60  | 18.95  |        | 1.400   | 1.050   |         | 1.225      |

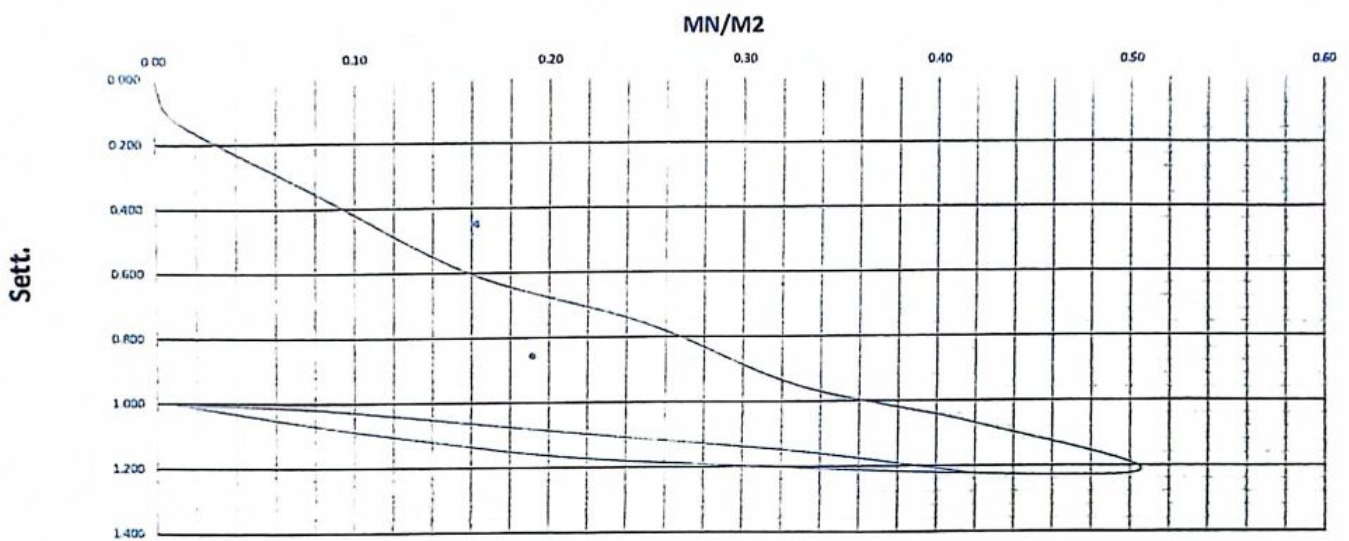
|                    |         | s       | AS      | Δσ  |
|--------------------|---------|---------|---------|-----|
| 0.7 σ <sub>1</sub> | 0.35    | 0.93438 | 0.36063 | 0.2 |
| 0.3 σ <sub>1</sub> | 0.15    | 0.57375 |         |     |
| 0.7 σ <sub>2</sub> | 0.35    | 1.17056 | 0.13555 | 0.2 |
| 0.3 σ <sub>2</sub> | 0.15    | 1.035   |         |     |
| D (mm)             | 300     |         |         |     |
| Ev <sub>1</sub>    | 124.78  |         |         |     |
| Ev <sub>2</sub>    | 331.97  |         |         |     |
| Area (Sq.m)        | 0.07065 |         |         |     |

|                                  |      |  |  |
|----------------------------------|------|--|--|
| Ev <sub>2</sub> /Ev <sub>1</sub> | 2.66 |  |  |
|----------------------------------|------|--|--|

$$E_v = 0.75 \cdot D \cdot \Delta \sigma / \Delta s$$

$E_v$  = deformation modulus  
 $\Delta \sigma$  = load increment  
 $\Delta s$  = settlement increment  
 $D$  = diameter of the plate, generally 0.30 m

For this calculation  $\Delta\sigma$  and  $\Delta s$  are usually taken from the load span between  $0.3 \sigma_{max}$  and  $0.7 \sigma_{max}$ .



Lab. Specialist

Name :

Sign :

Lab. Engineer

Name : Ahmed Hajeem

Sign :

Consultant Engineer

Name : Hassan

Sign :

## Plate Load Test Results

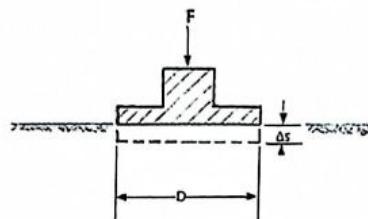
|              |                   |    |         |
|--------------|-------------------|----|---------|
| Company Name | AL ANOD           |    |         |
| Location     | 525+920           | To | 526+000 |
| Test Date    | 13-08-2023        |    |         |
| Layer level  | sub ballast +0.90 |    |         |

|         |         |
|---------|---------|
| Station | 525+995 |
|---------|---------|

### EQUIPMENT AND TEST PROCEDURE :-

The basis of the given equation is Boussinesq's theory of the relationship between the modulus of elasticity and the settlement of a circular rigid plate with the diameter  $D$ .

The load is applied to a circular rigid steel bearing plate by a hydraulic jack in several steps. The settlement under each load step is recorded. The following sketch shows the principle of the test.



$F$  = load

$\Delta s$  = settlement

$D$  = diameter of the plate

The diameter  $D$  of the plate is generally 0.30 m. For very coarse grained material also plates with diameter  $D = 0.60$  m and  $D = 0.762$  m are used

The load is applied in 6 load increments of equal size. Under each load step the settlement must come to a noticeable end ( $< 0.02$  mm/minute). After the maximum load is reached the unloading procedure can begin. After that, the plate is reloaded in 5 steps. A loaded truck, an excavator or a roller usually serve as counterweight for the hydraulic jack

Diameter = 300mm

| Loading   | Load  | Load   | Stress | Dial 1 | Dial 2 | Dial 3 | Sett. 1 | Sett. 2 | Sett. 3 | Avg. Sett. |
|-----------|-------|--------|--------|--------|--------|--------|---------|---------|---------|------------|
| Stage No. | Bar   | KN     | MM/M2  | mm     | mm     | mm     | mm      | mm      | mm      | mm         |
| 0.000     | 0.0   | 0.000  | 0.00   | 20.00  | 20.00  |        | 0.000   | 0.000   |         | 0.000      |
| 1.000     | 2.1   | 0.707  | 0.01   | 19.97  | 19.95  |        | 0.030   | 0.050   |         | 0.040      |
| 2.000     | 17.1  | 5.652  | 0.08   | 19.87  | 19.80  |        | 0.130   | 0.200   |         | 0.165      |
| 3.000     | 34.2  | 11.304 | 0.16   | 19.83  | 19.63  |        | 0.170   | 0.370   |         | 0.270      |
| 4.000     | 53.3  | 17.663 | 0.25   | 19.79  | 19.43  |        | 0.210   | 0.570   |         | 0.390      |
| 5.000     | 70.5  | 23.315 | 0.33   | 19.70  | 19.18  |        | 0.300   | 0.820   |         | 0.560      |
| 6.000     | 89.8  | 29.673 | 0.42   | 19.63  | 19.00  |        | 0.370   | 1.000   |         | 0.685      |
| 7.000     | 106.8 | 35.325 | 0.50   | 19.58  | 18.82  |        | 0.420   | 1.180   |         | 0.800      |
| 8.000     | 53.4  | 17.663 | 0.25   | 19.65  | 18.92  |        | 0.350   | 1.080   |         | 0.715      |
| 9.000     | 26.7  | 8.831  | 0.12   | 19.79  | 19.03  |        | 0.210   | 0.970   |         | 0.590      |
| 10.000    | 2.1   | 0.707  | 0.01   | 19.87  | 19.31  |        | 0.130   | 0.690   |         | 0.410      |
| 11.000    | 17.1  | 5.652  | 0.08   | 19.85  | 19.21  |        | 0.150   | 0.790   |         | 0.470      |
| 12.000    | 34.2  | 11.304 | 0.16   | 19.79  | 19.11  |        | 0.210   | 0.890   |         | 0.550      |
| 13.000    | 53.3  | 17.663 | 0.25   | 19.75  | 19.00  |        | 0.250   | 1.000   |         | 0.625      |
| 14.000    | 70.5  | 23.315 | 0.33   | 19.69  | 18.95  |        | 0.310   | 1.050   |         | 0.680      |
| 15.000    | 89.8  | 29.673 | 0.42   | 19.63  | 18.89  |        | 0.370   | 1.110   |         | 0.740      |

|                |         | s       | Δs      | Δσ  |
|----------------|---------|---------|---------|-----|
| 0.7 $\sigma_1$ | 0.35    | 0.58438 | 0.3275  | 0.2 |
| 0.3 $\sigma_1$ | 0.15    | 0.25688 |         |     |
| 0.7 $\sigma_2$ | 0.35    | 0.69333 | 0.16333 | 0.2 |
| 0.3 $\sigma_2$ | 0.15    | 0.53001 |         |     |
| D (mm)         | 300     |         |         |     |
| $E_{v1}$       | 137.40  |         |         |     |
| $E_{v2}$       | 275.52  |         |         |     |
| Area (Sq.m)    | 0.07065 |         |         |     |

|                 |      |  |  |
|-----------------|------|--|--|
| $E_{v2}/E_{v1}$ | 2.01 |  |  |
|-----------------|------|--|--|

$$E_v = 0.75 \cdot D \cdot \Delta \sigma / \Delta s$$

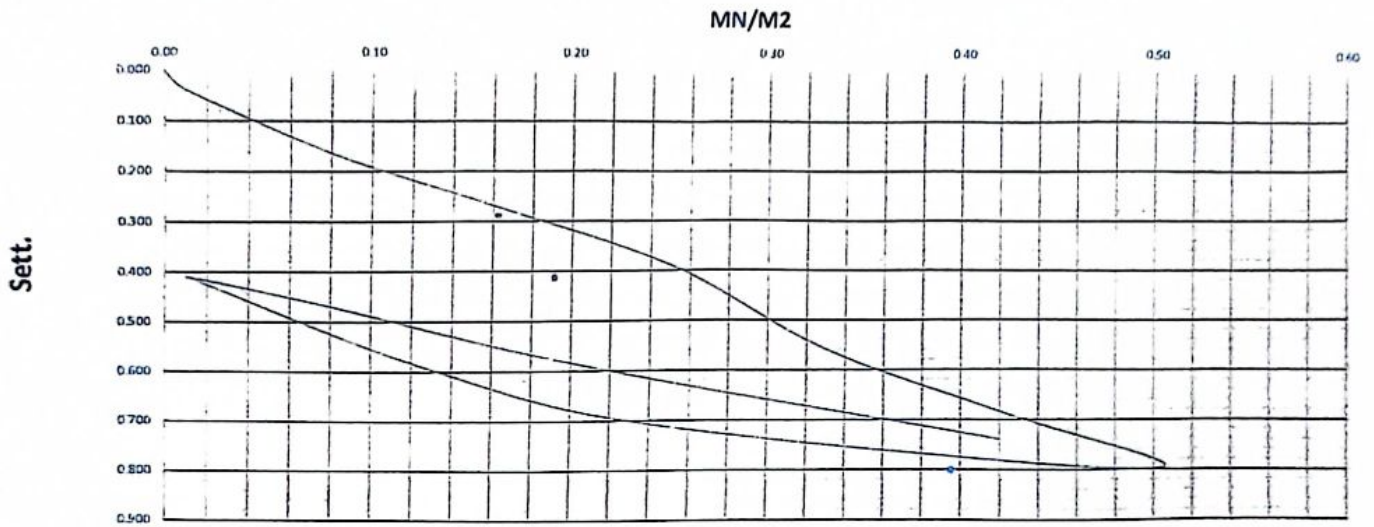
$E_v$  = deformation modulus

$\Delta \sigma$  = load increment

$\Delta s$  = settlement increment

$D$  = diameter of the plate, generally 0.30 m

For this calculation  $\Delta\sigma$  and  $\Delta x$  are usually taken from the load span between  $0.3 \sigma_{max}$  and  $0.7 \sigma_{max}$ .



**Lab. Specialist**

Name :

Sign :

**Lab. Engineer**

Name : Ahmed Haleem

Sign :

**Consultant Engineer**

Name : Hassan

Sign :